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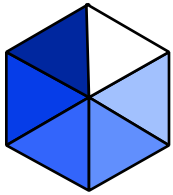
Design and Development of Piezoelectric Actuators and Motors at Garman Systems

Prepared by:

Garman Systems inc.

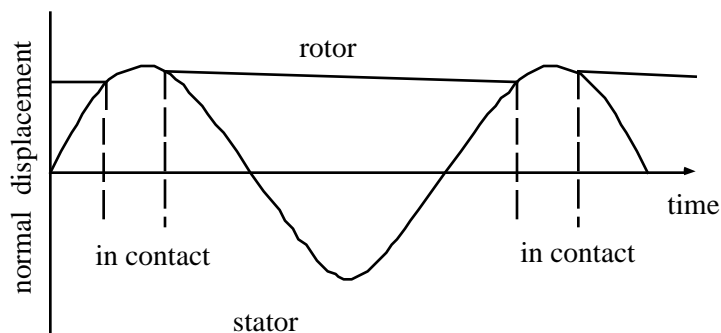
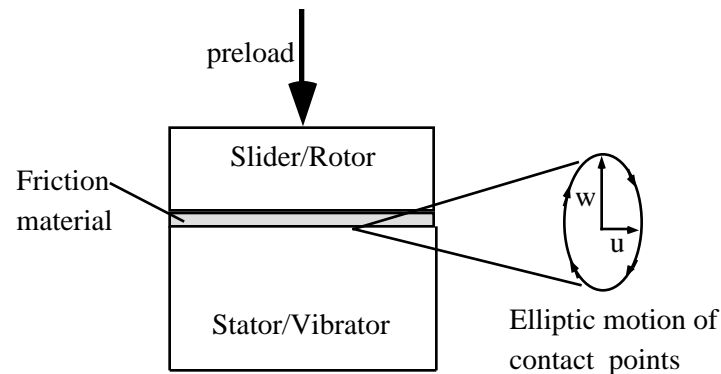
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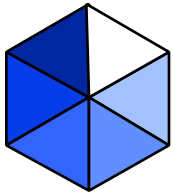


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Resonant (Ultrasonic) Motors

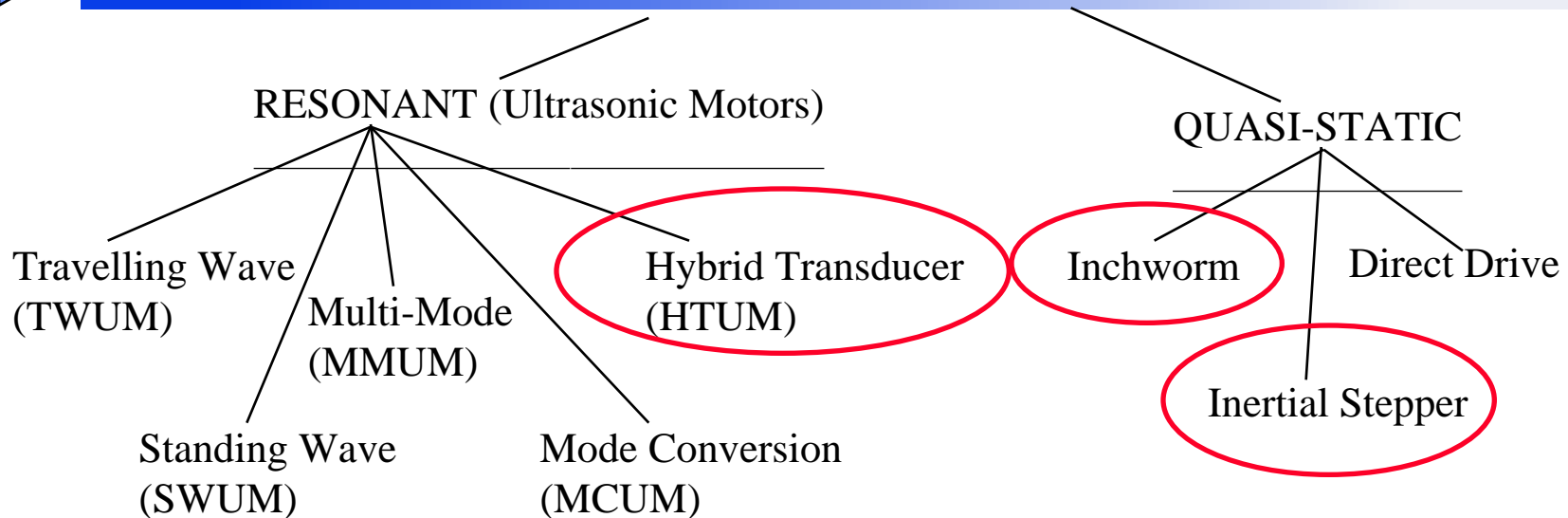


- ▶ Piezoelectrics generate an elliptic motion on the surface of the stator.
- ▶ A rotor/slider is pressed to the stator.
- ▶ Because of the difference in time constants, the rotor is contacted intermittently.
- ▶ The slider is driven by the tangential motion of the ellipse.
- ▶ The force is determined by friction and the normal component of the ellipse.
- ▶ Velocity and direction are controlled by phase or voltage.

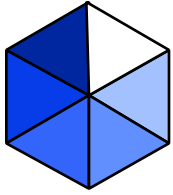


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GSi Motor Concepts



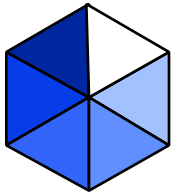
- | Inchworm
 - Designed in ability to operate at high frequency w/o wear
 - Uses high stroke piezo clamping devices to compensate for wear and tolerances
- | Stick/Slip Stepper Motor (modified inertial stepper)
 - Kinetic - Static friction drive
- | Hybrid transducer ultrasonic motor (HTUM)
 - Designed with micro-positioning capability



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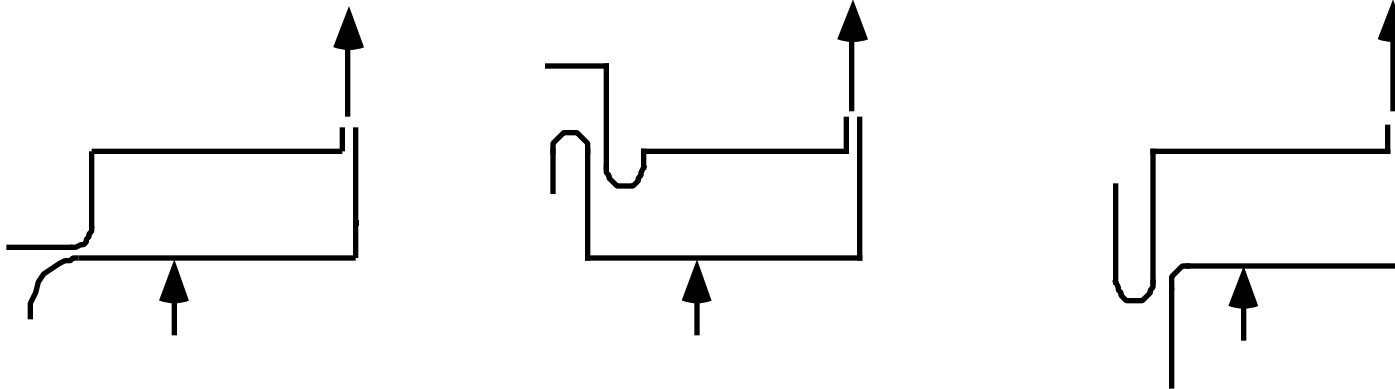
The need for amplification

- ▶ Piezoelectric stacks have high force, high resonance frequency, and high power density, but very small stroke
 - u The stacks have a blocked force of 850 N and a resonance frequency of 7 kHz
 - u The stacks can produce strains of 0.1%
- ▶ The segment requires 100 μ m of piston motion, this would necessitate a 100mm tall stack
- ▶ Amplification flexure mechanisms can increase the motion of the stack to the required level

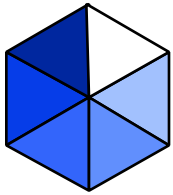


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Optimal Flexure Orientation

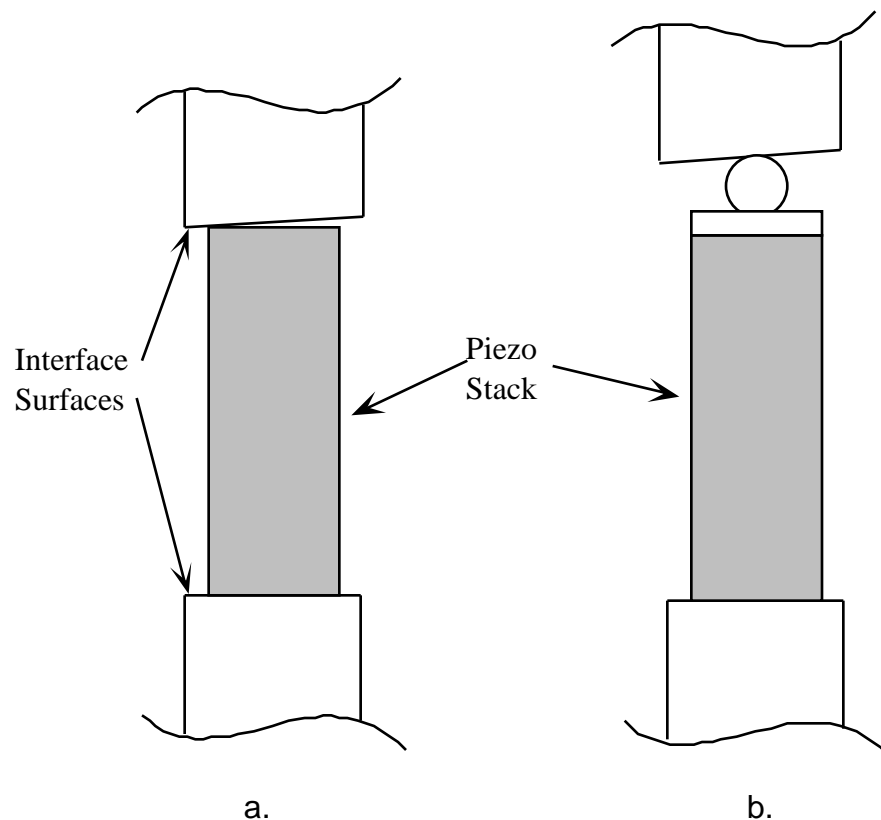


- When input force is applied, flexure is put in:
 - Case 1. Shear
 - Case 2. Compression
 - Case 3. Tension
 -
- Through an iterative process, Case 3 has been proven to be most efficient for our flexure mechanisms

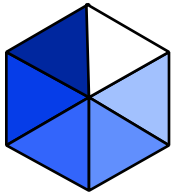


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Flexure-Stack Mechanical Interface

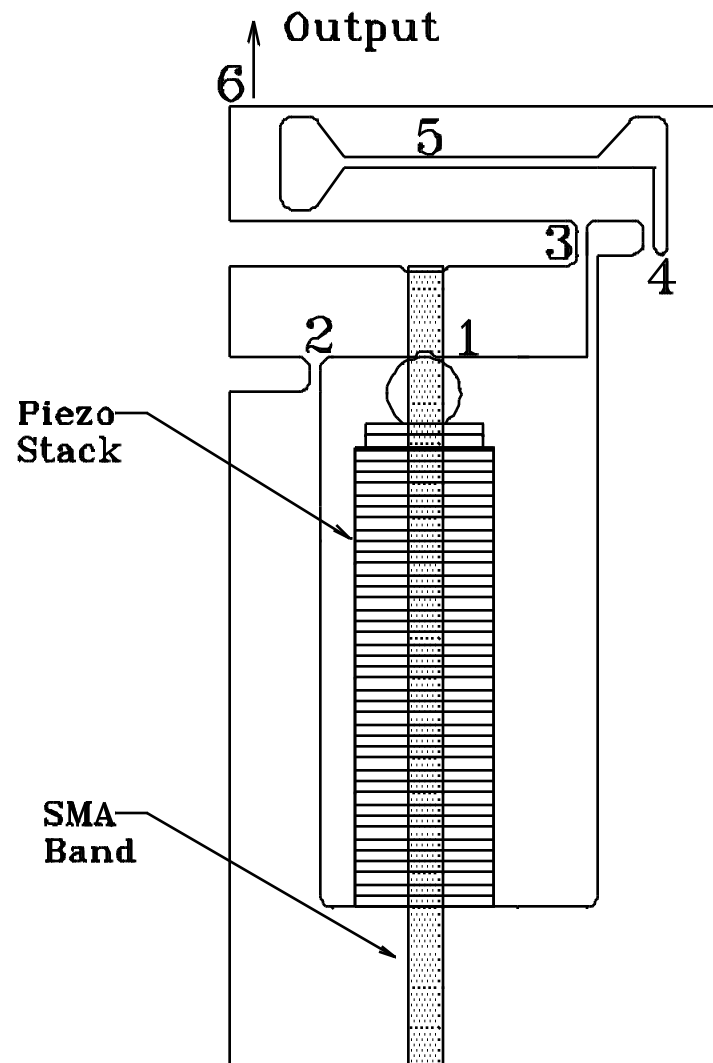


- ▶ Piezo stacks work best when subjected to compressive loads applied vertically to the center of the stack
- ▶ Loads applied off-center can damage the stack
- ▶ A steel sphere provides an ideal interface
 - u The sphere keeps loads applied on the center axis of the stack
 - u The sphere is not affected by small surface variations where the stack interfaces the flexure

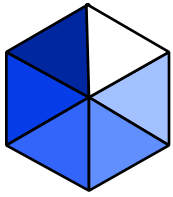


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Flat Plate Mechanism

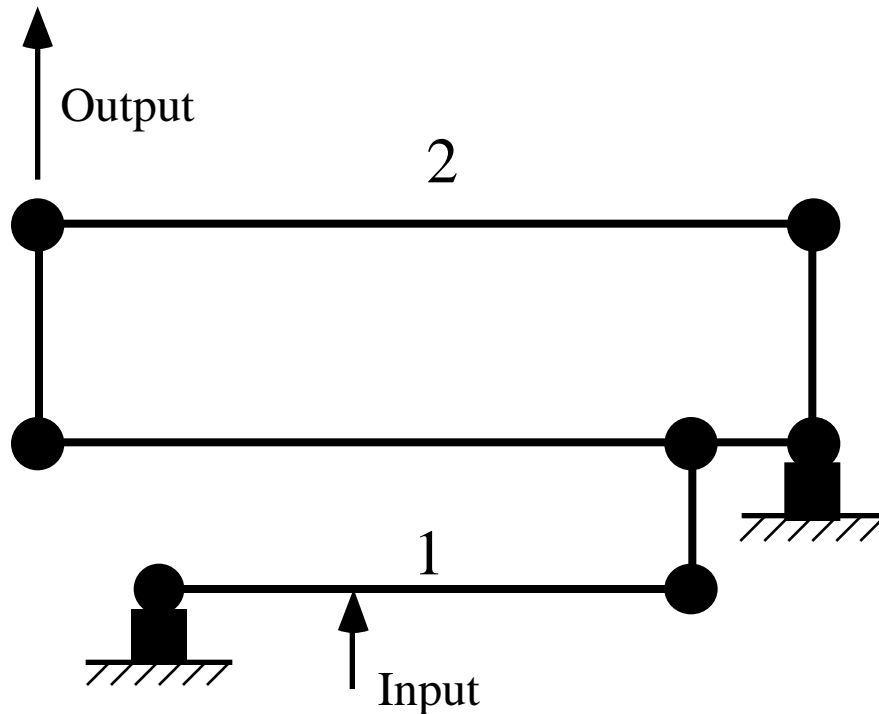


- The detail shown is cut with a wire EDM machine
-
- Critical dimensions:
- Height: 45.5 mm
- Width: 30 mm
- Thickness: 5 mm

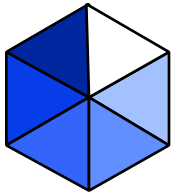


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Kinematic Analysis

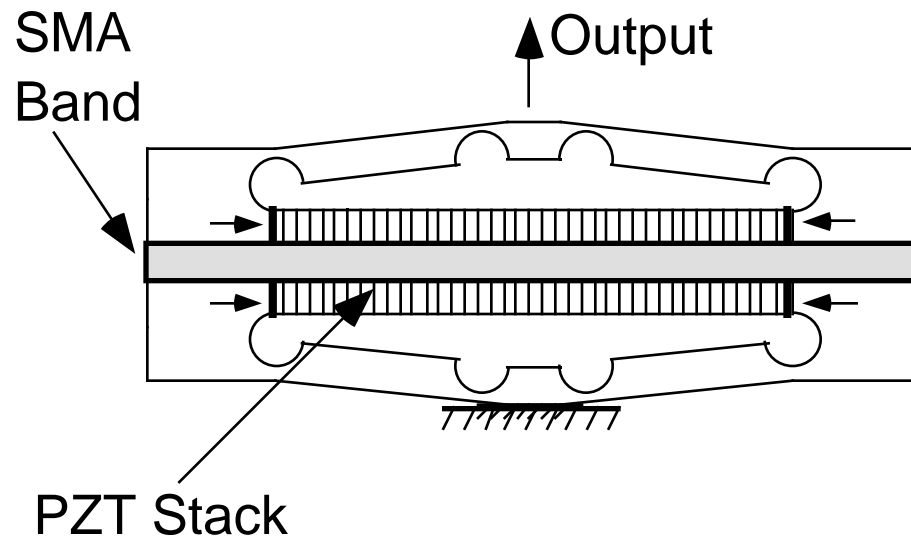


- The linkages are considered to be rigid bodies for kinematic analysis
-
- Stages 1 and 2 are cantilevered beams
-
- Stage 2 contains a four bar parallel linkage, to insure vertical motion
-
- The ideal kinematic amplification factor of the flat plate mechanism is 12.7

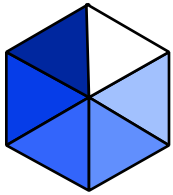


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BOA Mechanism

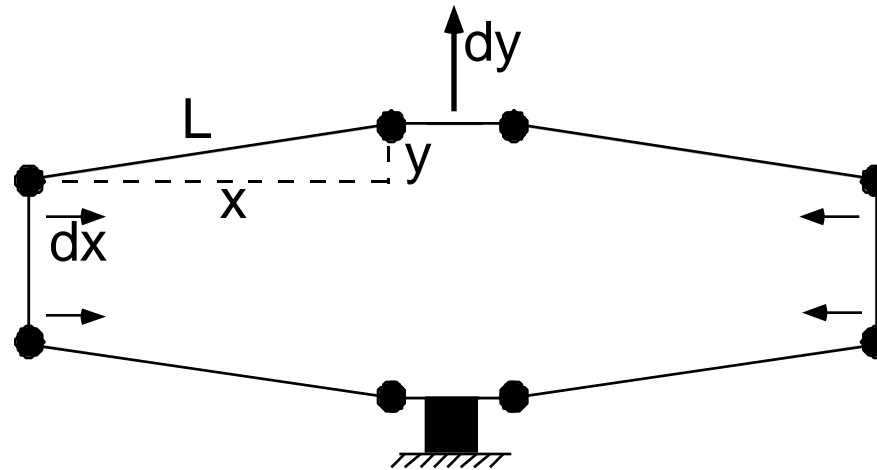


- | The mechanism is cut from a single piece of steel using wire EDM
-
- | The output displacement is controlled by the expansion of the piezo stack
-
- | Output force is dependent on the SMA band and the stiffness of the flexure
-
- | Critical dimensions:
 - u Length: 27 mm
 - u Height: 11 mm
 - u Depth: 5 mm



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Kinematic Analysis



- | The linkages are considered to be rigid bodies for kinematic analysis

-

- | The equation governing the ideal output is:

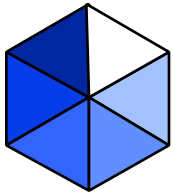
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$$dy = \frac{x}{y} dx$$

-

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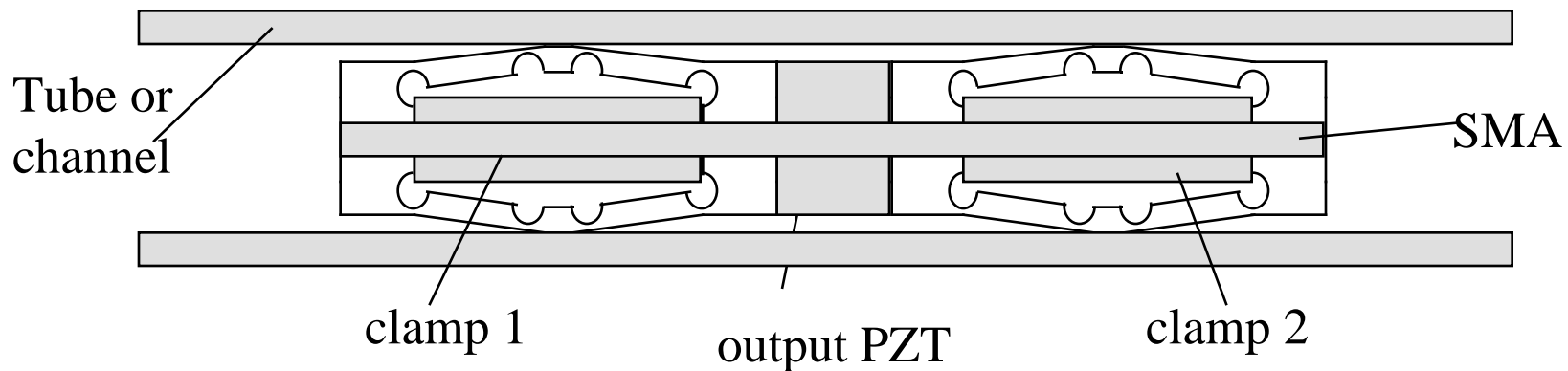
- | The kinematic amplification factor is 9X for the configuration shown

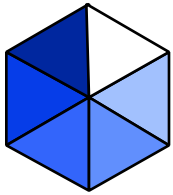


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BOA Inchworm (in channel)

- ▲ Use BOA type actuator to get clamping motion
 - u Compact clamping actuator with minimal non-active material
 - u Long stroke of BOA allows compensation for manufacturing tolerance and thermal expansion/contraction
- ▲ Design offers limited ability to make electrical or mechanical adjustments

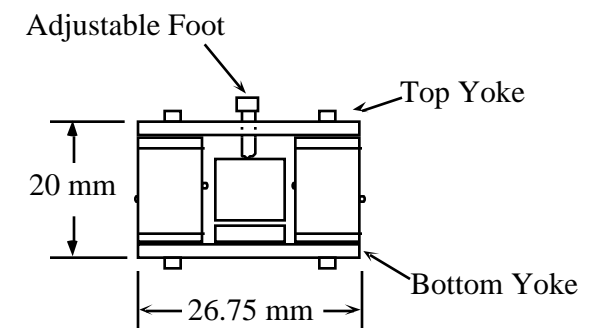
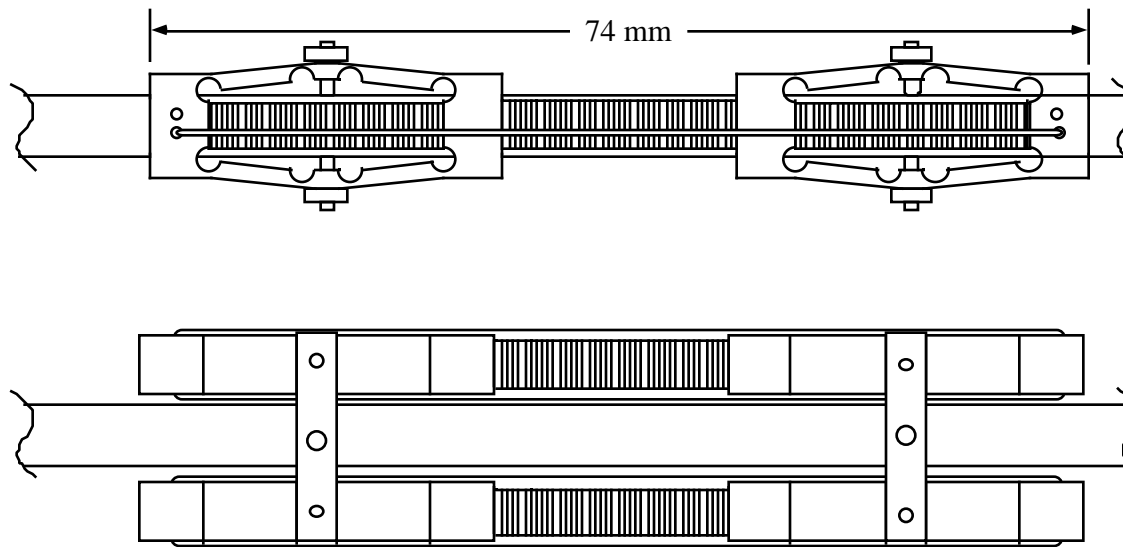


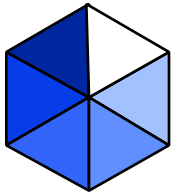


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BOA Inchworm (on shaft)

- ▲ Pairs of BOA type actuators mounted around a shaft
 - u Each pair of BOAs connected with top and bottom yokes
 - u Adjustable foot used to compensate for manufacturing tolerances and thermal expansion/contraction
- ▲ Longer extension stacks yield larger step sizes and greater motor speed



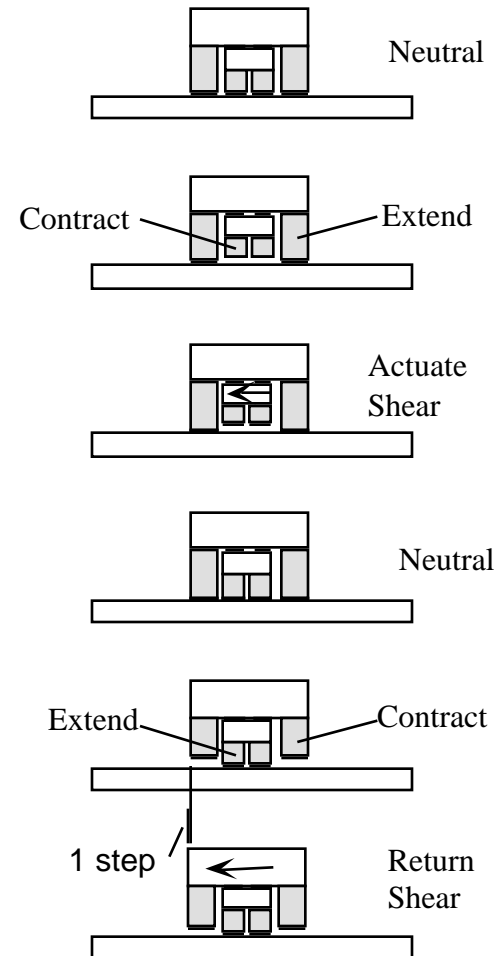
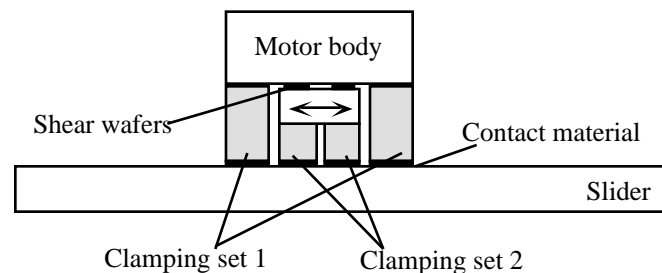


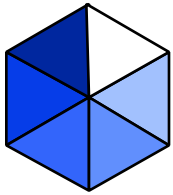
GSi Differential Stroke Inchworm Motor

▲ Eliminate assembly tolerance issue

- u preload a “stator” to a shaft
- u rely on the difference between the extension and contraction of stack actuators
- u wear is automatically compensated for
- u can be run at high frequency

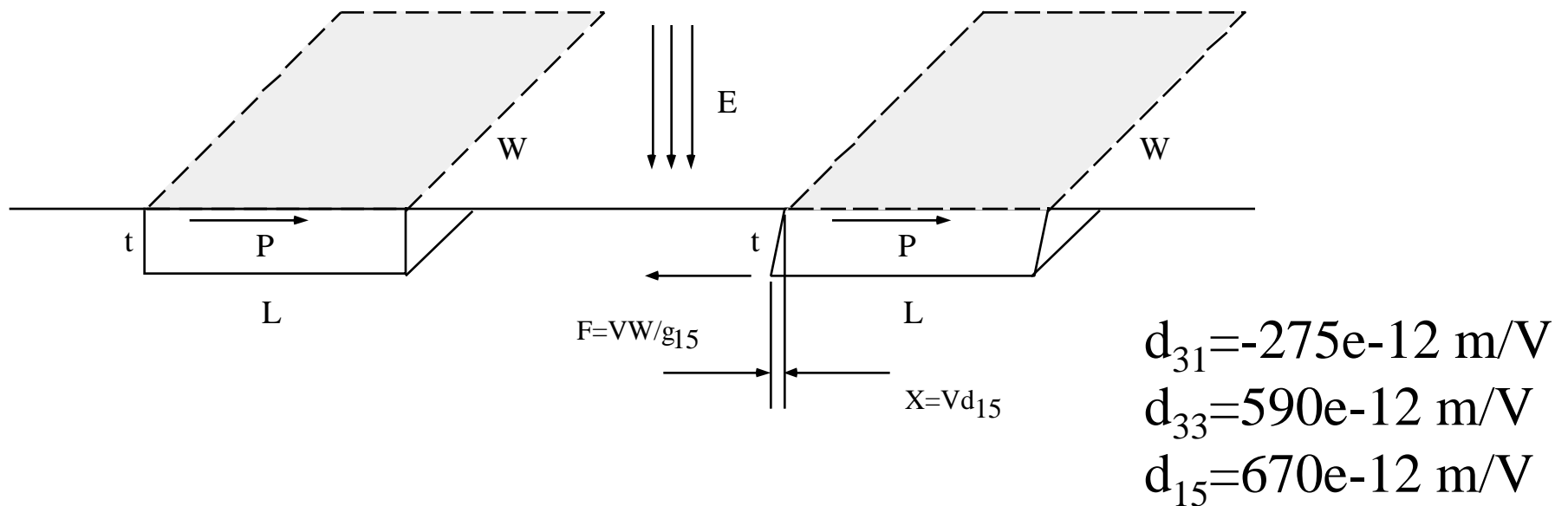
▲ Use shear wafers for output





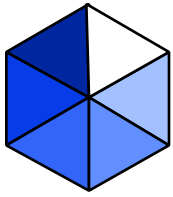
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Piezoelectric Shear Wafer



Advantages of shear wafers

- u High positive and negative voltage limits
 - ▲ Limited by the dielectric breakdown in both directions
- u Does not depole easily, minimal aging.
- u Can be stacked.



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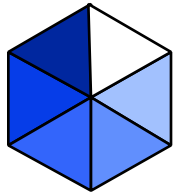
Scalability Considerations for Inchworm Motors

▲ Tolerance and assembly

- u Static displacement of a piezo-actuator is used for clamping and releasing
- u Dimensional tolerances must be less than the maximum stroke of the piezo-actuator
 - ▲ The slider/clamp interface must be “smooth” in order to avoid stalling
- u Lever arm stroke amplification mechanisms have be used to address these limitations on miniaturization

▲ Wear

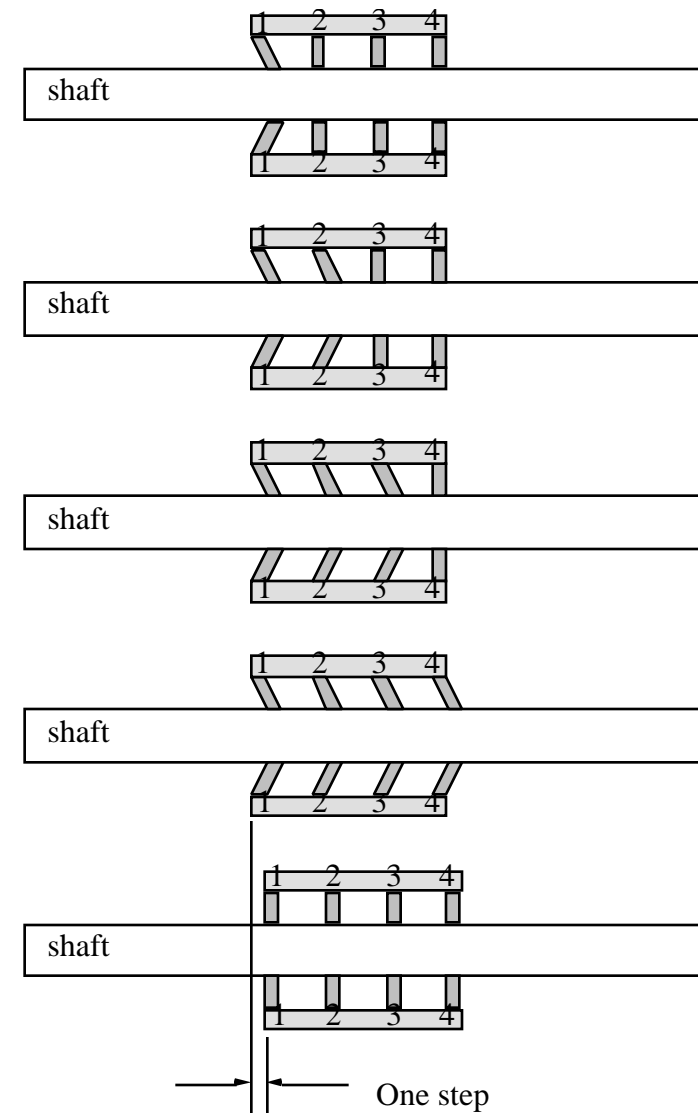
- u Operation well below resonance minimizes wear
 - ▲ higher frequency operation introduces dynamics of the clamping and extension mechanisms and increases wear
 - ▲ Small motors can be operated at high frequency with out exciting motor dynamics
- u Differential stroke compensates for wear through preload

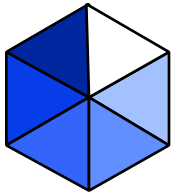


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Stick/Slip Stepper - Operating Principle

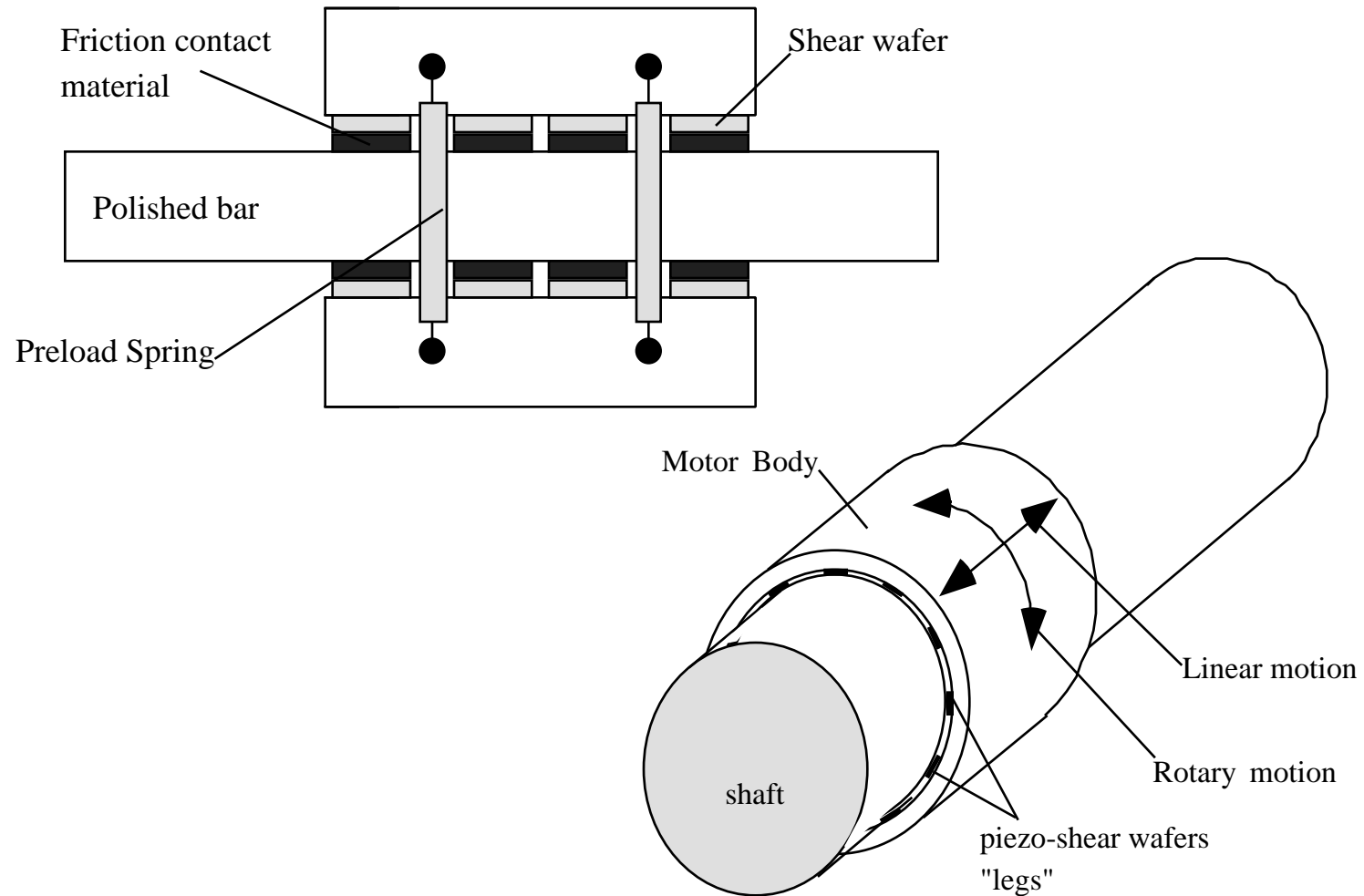
- ▶ Piezo shear wafers operate in sequence shown
- ▶ Single leg moves because kinetic friction is less than holding force of other legs (kinetic < static)
- ▶ Precision micro-positioning accomplished by activating all legs together
- ▶ Shear wafers can be stacked to improve speed at the cost of force (displacement per cycle increases)

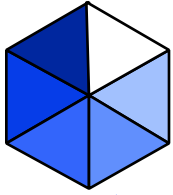




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Stick/Slip Stepper Motor

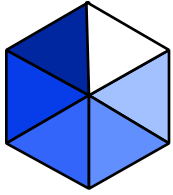




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Stick/Slip Stepper Design Issues

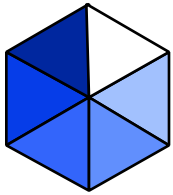
- ▶ Contact uniformity is critical
 - u can be addressed through the use of a compliant backing
- ▶ Amplifier slew rate
 - u high slew rate is required to ensure that the feet break into kinetic friction
- ▶ Contact material choice is critical
 - u high static friction coefficient & low kinetic friction coefficient
- ▶ Can be made completely non-magnetic
 - u ceramic or plastic body, run on a ceramic shaft
- ▶ Simple design makes this motor very scaleable
- ▶ Potentially low cost, versatile linear motor
 - u provided that further development research proves successful



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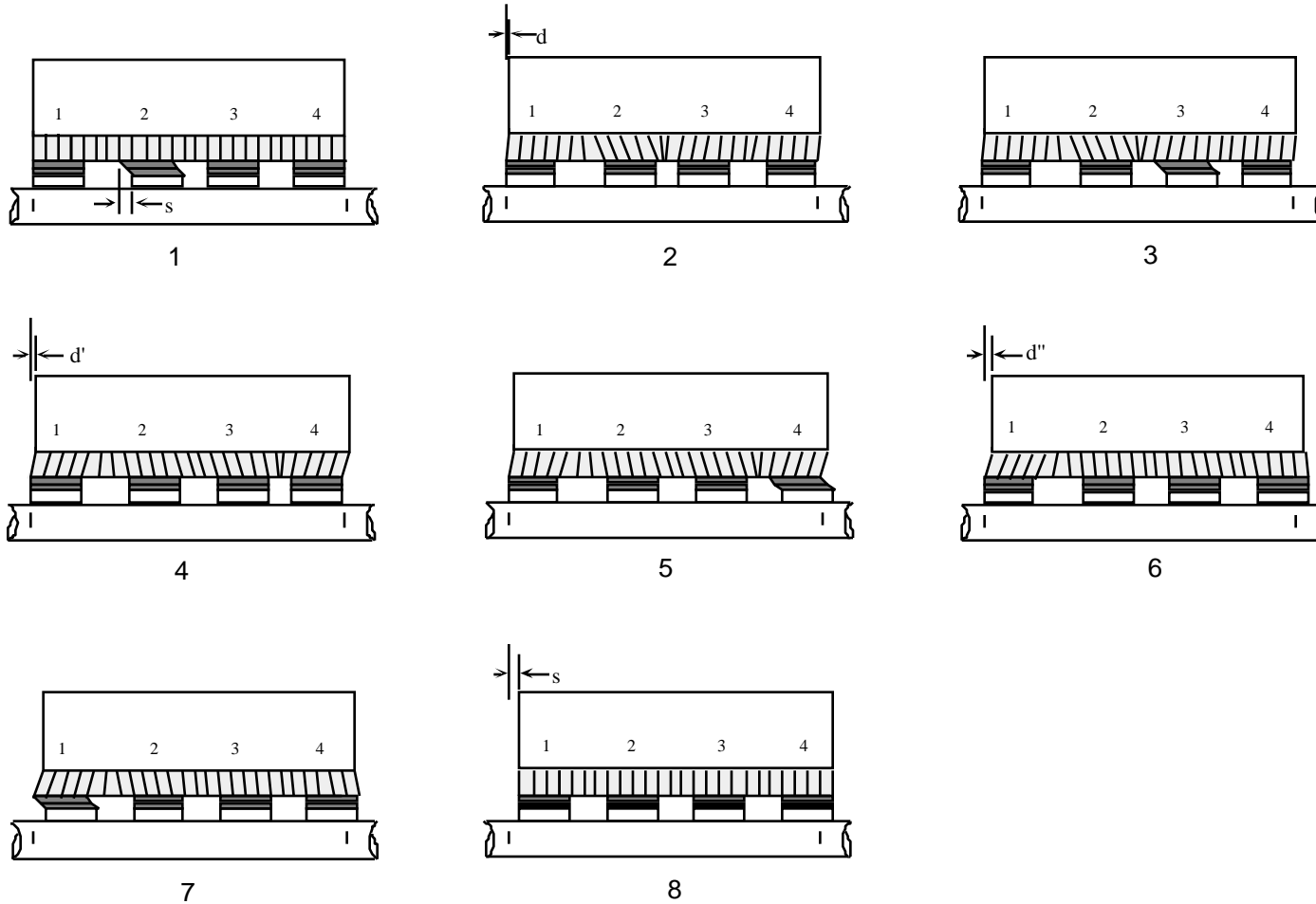
Pharaoh's Motor

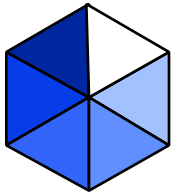
- ▲ Utilizes strain in an elastic medium to store energy.
- ▲ Force and displacement of each individual actuator accumulate to provide smooth motion for the motor.
- ▲ Force required from individual actuator is much less than force output of the motor.



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Pharaoh's Motor stepping sequence

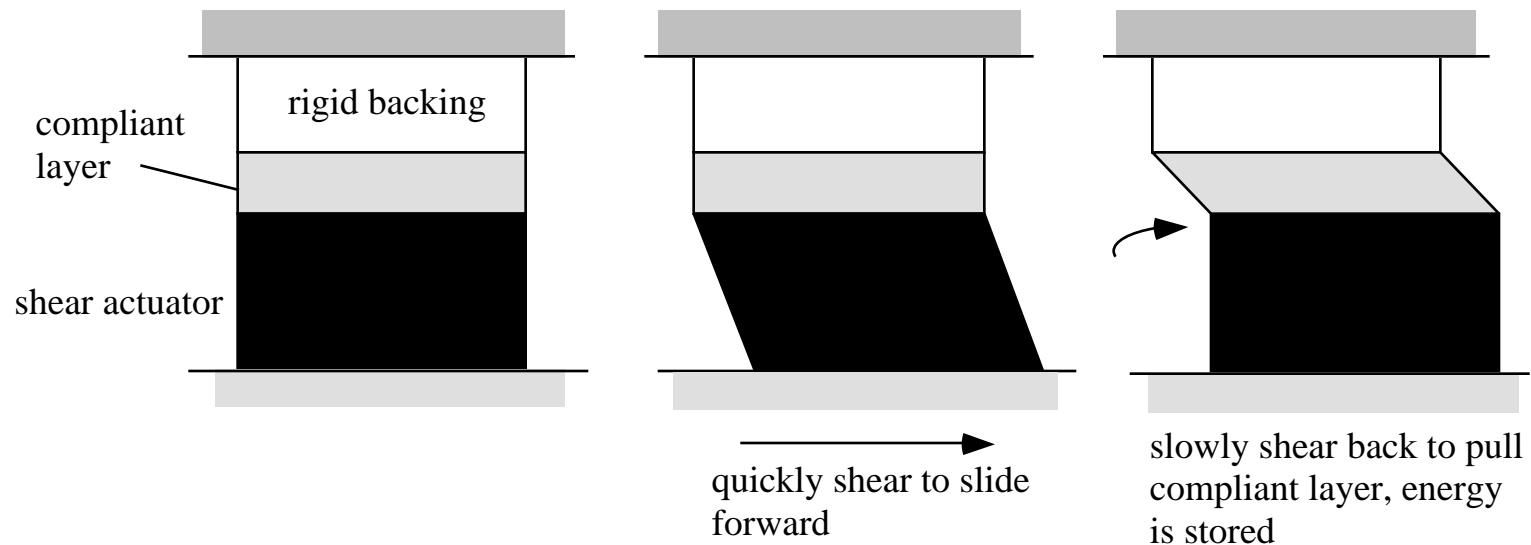


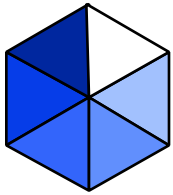


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Pharaoh's Motor

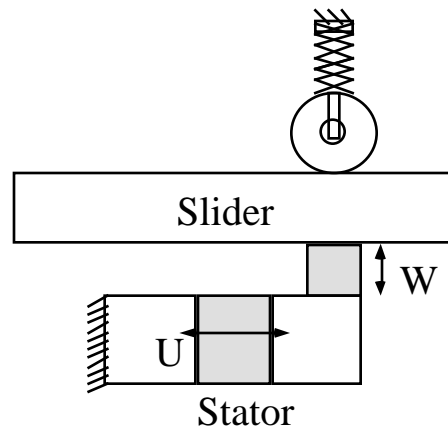
▲ Feasibility study of one Pharaoh's motor 'foot'



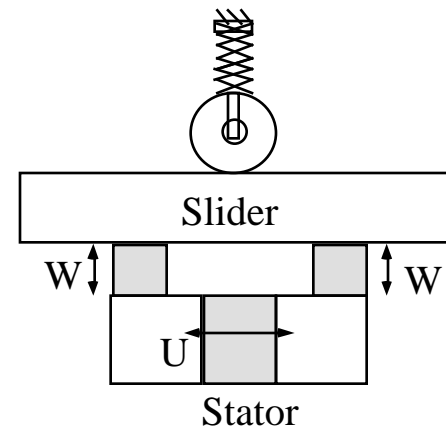


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Hybrid Transducer (HTUM)

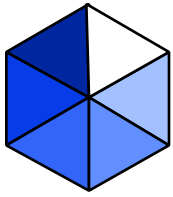


One contact point



Two contact points

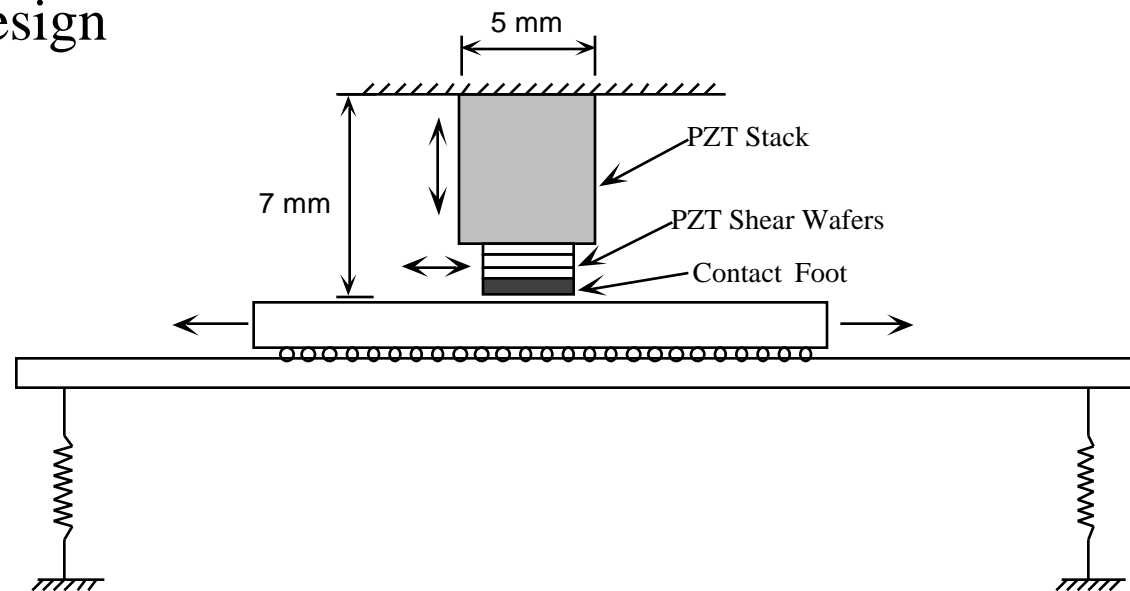
- | Elliptic motion is generated by two orthogonal piezo-vibrators
- | Operate at resonance of output, U
- | Separation of elliptic motion into two controllable components allows performance and design flexibility
- | Easier to miniaturize
- | Can tune both resonance frequencies to get best performance

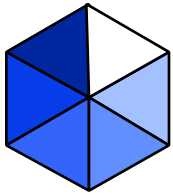


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Shear Stack HTUM

- ▶ Elliptical motion is created using shear wafers, and a linear stack actuator, running 90° out of phase
 - u The linear stack is 5 x 5 x 5 mm, capable of displacing $4\mu\text{m}$
 - u 4 shear wafers are hand stacked
- ▶ The contact foot is covered with Kapton film to prevent ultrasonic welding
- ▶ Resonant frequencies above 20 kHz because of its low mass
- ▶ Extremely compact design

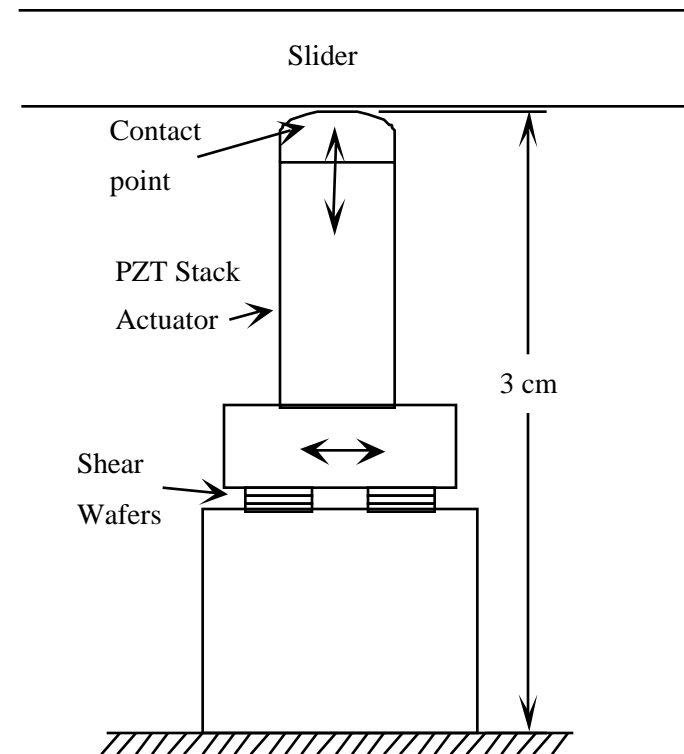


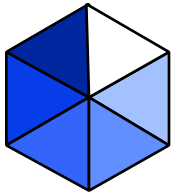


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Modified Shear Stack HTUM

- ▶ The added mass that the shear wafers move lowers the resonant frequency
- ▶ The linear stack actuator is 10x5x5 mm, capable of displacing 9 μm
- ▶ Two shear stacks provide horizontal motion
- ▶ The resonant frequency is lower than 20 kHz, the maximum frequency that can be achieved with the quadrature oscillator chip





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Modified Shear Stack HTUM: Test Results

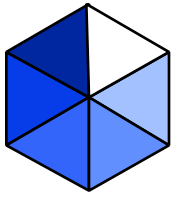
▲ The stator was placed on a translation stage and pushed against a slider mounted on compression springs for testing

▲ Results:

- u Frequency: 18.1 kHz
- u Shear stack input: 92 Vpp
- u Linear stack input: 39 Vpp
- u Static holding force: 4.4 N

<u>Load (N)</u>	<u>Speed (mm/s)</u>
Unloaded	32
0.49	22
0.98	12

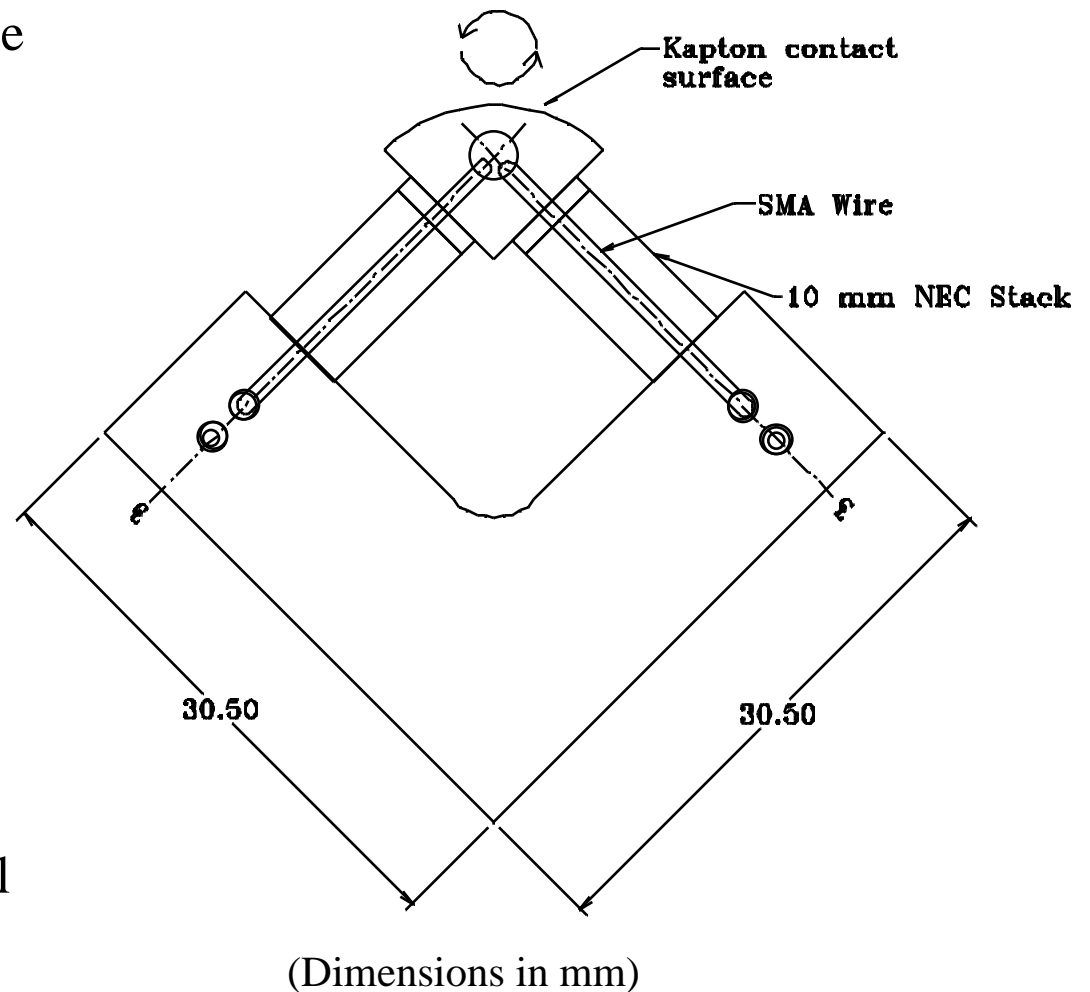
▲ Increased performance can be achieved by operating multiple stators in parallel

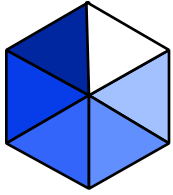


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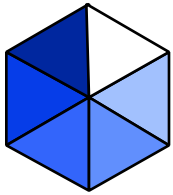
Orthogonal Stack HTUM

- ▶ Operation of the stack actuators with sine waves 90° out of phase creates elliptical motion at the contact point
 - u The input signal is generated by a quadrature oscillator chip
- ▶ The stack actuators can achieve a $9\mu\text{m}$ displacement with a voltage input of 150 Vpp
- ▶ The stack actuators are held in place using super-elastic Nitinol





- ▶ The principle of operation is the same as in the orthogonal stack HTUM, with the addition of the BOA mechanism
- ▶ The BOA mechanism provides amplification, increasing speed and load carrying capability
 - u The BOA mechanism increases the stepsize of the motor
 - u Steel BOAs are used for increased stiffness
 - u The BOAs are preloaded with superelastic Nitinol
- ▶ Because of the amplification, the resonant frequency is much lower than with the other HTUMs
- ▶ The BOA HTUM is run as the orthogonal stack motor with two sine waves 90° out of phase



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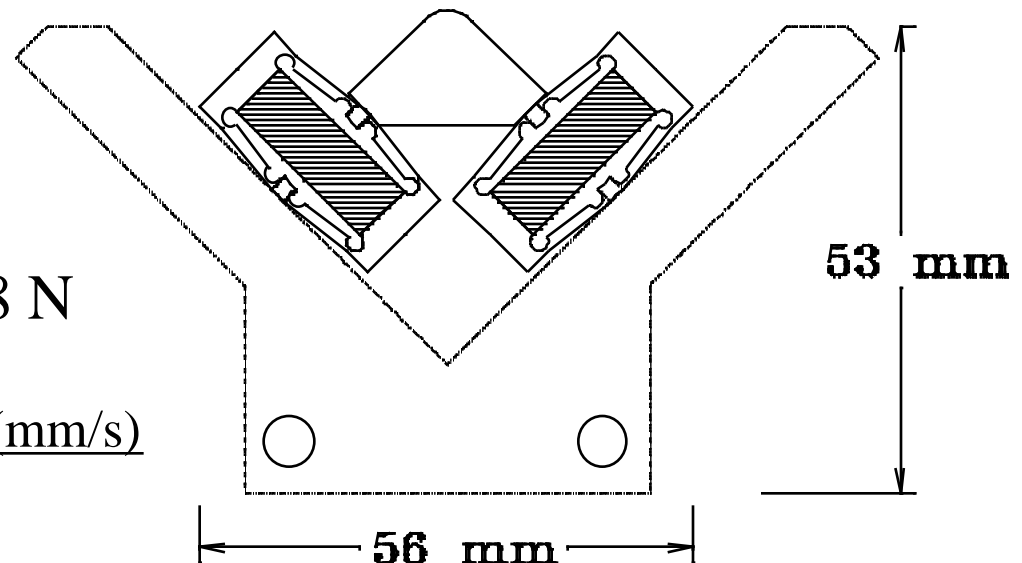
BOA HTUM: Test Results

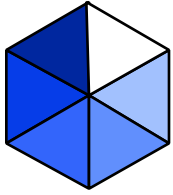
▲ The BOA HTUM is run by advancing the motor with a translation stage to contact a slider mounted on compression springs

▲ Results:

- u Frequency: 1kHz
- u Input: 80 Vpp
- u Static holding force: 9.8 N

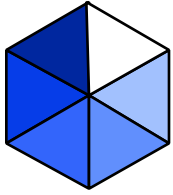
<u>Load (N)</u>	<u>Speed (mm/s)</u>
Unloaded	13
0.49	10
1.47	3.7
2.45	2.2





GSI HTUM Future Development Issues

- ▶ The motors operate best at resonance, but the frequency of the resonance changes with the motor normal force, temperature, and operating voltage
- ▶ Accurate analysis of the movement of the contact point of the stator and the slider requires a measurement system such as a laser vibrometer
- ▶ A higher frequency quadrature oscillator will be needed for miniaturization
- ▶ The HTUMs can operate with multiple stators
- ▶ The prototypes built show potential for several different designs



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Summary

- ▲ Garman Systems has diverse experience in piezoceramic based actuators and motors
 - u Axial and transverse flexure based actuators
 - u Linear and rotary inchworm designs
 - u Stick/slip motor designs
 - u HTUM designs
- ▲ The Pharaoh's motor represents a novel piezoelectric drive mechanism
 - u work in progress